

Local Avalanche Effect of 4H-SiC p-i-n Ultraviolet Photodiodes With Periodic Micro-Hole Arrays

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Abstract—In this report, 4H-SiC p-i-n photodiodes with various micro-hole arrays are fabricated, then measured and discussed by using photoelectric measurement system and simulation software. Periodic micro-hole arrays etched from p layer to i layer are obtained by using the selective etching technology, which increases the photosensitive area of devices and reduces the ultraviolet light absorption of p layer. The average dark current of devices has an ultralow value of approximate 6.0×10^{-15} A in the low reverse bias range of 0-10 V. Furthermore, the device with 4 μm micro-hole exhibits the best performance and its peak responsivity increased by 10.4 % compared to the conventional device. It is significant that the peak responsivity and corresponding external quantum efficiency of devices with 4 μm micro-hole at 40 V bias are 815 % and 819 % higher than those of devices without micro-hole, respectively. This is attribute to the fact that a high electric field is observed around the micro-holes as the reverse bias increased to 40 V, which leads to local avalanche. Thus, the local avalanche photodiodes work at a relatively low bias, which improved the responsivity and quantum efficiency of the device enormously.

Index Terms—4H-SiC, ultraviolet, photodiodes, micro-hole.

I. INTRODUCTION

ULTRAVIOLET (UV) photodiodes (PDs) have attracted much attention owing to their extensive applications such

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as environmental monitoring, space science, UV communication and biological agent detection [1]–[3]. Taking advantages of its large bandgap energy, superior thermal conductivity, and high electron saturation velocity, SiC performs as an attractive candidate material to fabricate solar-blind PDs [4]. SiC UV PDs with various structures, such as schottky, p-i-n, metal-semiconductor-metal (MSM), and avalanche, have been developed to satisfy all kinds of applications [5]–[9].

However, the responsivity of SiC-based PDs is still lower than expected and need to be improved for weak UV signals detection. In recent years, many methods have been proposed to improve the performance of UV PDs. For instance, microlens arrays were fabricated on the SiC PDs to enhance the absorption efficiency of light [10]–[12]. The thinner p layer was also used to improve the spectral response of SiC p-i-n UV PDs [13]. Porous structure etched on the device surface by electrochemical method enhanced the surface roughness and reduced light reflection [14]–[16]. The nanohole and nanorod arrays were also used to improve the performance of the detectors owing to their light trapping [17], [18]. However, fabrication of microlens is a complex process and its cost is expensive. Electrochemical etching will increase the dark current of the device, and the size of pores is difficult to control. The micro-hole array structure is also a feasible method, which has been applied in solar cells to improve light absorption [19], [20].

In this work, 4H-SiC p-i-n UV PDs with periodic micro-hole arrays are fabricated. The effects of micro-hole arrays with various diameters on the performance of 4H-SiC PDs are discussed in detail by photoelectric measurements and Technology Computer Aided Design (TCAD) simulation.

II. DEVICE STRUCTURE AND FABRICATION

Fig. 1 (a) shows the schematic diagram of the 4H-SiC device with micro-hole arrays. The 4H-SiC epitaxial structure consists of a 200-nm-thick p⁺ layer ($N_A = 1 \times 10^{19} \text{ cm}^{-3}$), a 3000-nm-thick i layer ($N_D = 1 \times 10^{15} \text{ cm}^{-3}$) and a 500-nm-thick n layer ($N_D = 2 \times 10^{18} \text{ cm}^{-3}$). Fig. 1(b) shows the top-view photograph of fabricated micro-hole array with p electrode. The photoactive window area of the detector is $200 \times 200 \mu\text{m}^2$. Prior to device fabrication, TCAD simulation are performed to analyze the influence of micro-hole on device performance. The devices are simulated using a plane 2-D structure, and the thickness and doping concentration are confirmed with the Fig. 1(a). TCAD solves the continuity and Poisson's equation for the charge carriers [21]. The default parameters are used for the concentration-dependent

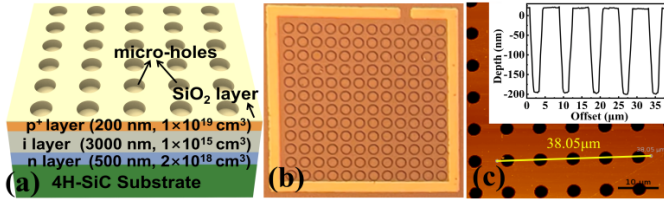


Fig. 1. (a) The schematic structure of 4H-SiC device with micro-hole array. (b) The top-view photograph of fabricated micro-hole array with p electrode. (c) Surface morphology of micro-holes with 3 μm in diameter measured by AFM and the corresponding cross-sectional profile shown in the inset.

lifetime, Shockley-Read-Hall (SRH) recombination and for concentration and field dependent mobility models.

Firstly, a beveled mesa of device was processed by photoresist reflow technology to effectively suppress the edge breakdown of the device. Then, a standard photolithography process is used to obtain the micro-hole array patterns by using AZ5214E positive photoresist. Five kinds of micro-hole diameters ($D = 3, 4, 6, 8,$ and $10 \mu\text{m}$) were prepared, and the micro-hole spacing is fixed to $5 \mu\text{m}$. Subsequently, the inductive coupled plasma (ICP) etching was performed with a gas flow rate of $30 \text{ sccm} (\text{CF}_4)/5 \text{ sccm} (\text{O}_2)$. The etching time was 250s, corresponding to a predicted etching depth of $210 \pm 10 \text{ nm}$. Then, a lift-off process is applied to obtain the micro-hole array. Atomic force microscope (AFM) was employed to characterize the shape and size of the micro-holes as shown in Fig. 1(c). The micro-holes show a good uniformity and the etching depth of micro-holes is almost same as 220 nm, indicating that micro-holes are etched to the underlying i layer, which meet with the requirements of devices.

Then, an approximate 45-nm-thick SiO_2 was deposited, which is beneficial to reduce the surface dark current of the device and suppress the edge breakdown of micro-hole. $\text{Ti}(40 \text{ nm})/\text{Al}(60 \text{ nm})/\text{Ti}(10 \text{ nm})/\text{Au}(100 \text{ nm})$ and $\text{Ti}(5 \text{ nm})/\text{Ni}(200 \text{ nm})/\text{Ti}(5 \text{ nm})/\text{Au}(150 \text{ nm})$ metals were sputtered on the p^+ layer and the backside of n^+ substrate, respectively, followed by rapid thermal annealing in Ar ambient at $1000 \text{ }^\circ\text{C}$ for 2 min to form Ohmic contacts. As a final step, $\text{Ti}(20 \text{ nm})/\text{Au}(300 \text{ nm})$ was sputtered as wire-bonding pad. For comparison, the traditional 4H-SiC p-i-n PDs without micro-holes were also fabricated by using the same process. Keithley 4200 analyzer was used to obtain the current-voltage (I-V) characteristics of devices. A Xenon lamp as the light source was connected with a monochromator for single wavelength selection to measure the spectral response.

III. RESULTS AND DISCUSSION

Fig. 2(a) and (b) show the dark current and photocurrent characteristics of devices with and without micro-hole. The average dark currents of PDs were ultralow about $6 \times 10^{-15} \text{ A}$ in the reverse bias range of 0-10 V. The dark currents of device with micro-holes show no significant increase, which is attributed to the dark current effectively restrained by the oxide layer deposited on the micro-holes. Fig. 2(b) indicates that the photocurrents of devices with micro-holes ($D = 3$ and $4 \mu\text{m}$) are larger than that without micro-holes, however, the photocurrents of devices with micro-holes ($D = 6, 8,$

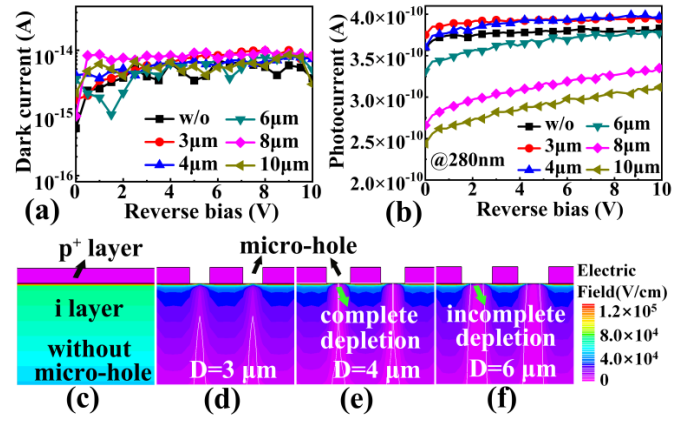


Fig. 2. The reverse current-voltage of devices with and without micro-hole (a) under dark on a log scale and (b) under the illumination of 280 nm on a linear scale. TCAD simulations of electric field intensity distribution in depletion region at 10 V bias for devices (c) without micro-hole, (d) with 3 μm micro-hole, (e) with 4 μm micro-hole and (f) with 6 μm micro-hole.

and $10 \mu\text{m}$) have a significant decrease. This phenomenon that photocurrent increases first and then decreases as the micro-hole diameter increases, which is mainly due to the absorption layer at the micro-hole cannot be completely depleted when the micro-hole diameter is larger than a certain value ($D \geq 6 \mu\text{m}$). Therefore, as the micro-hole diameter less than this certain critical value, the absorption layer at the micro-hole can be completely depleted, thus the photocurrents of the devices with micro-hole are significantly greater than the device without micro-hole.

Fig. 2(c)-(f) show electric field intensity distribution in depletion region of devices with and without micro-holes simulated by TCAD. The devices without micro-hole and with micro-holes ($D = 3$ and $4 \mu\text{m}$) can be completely depleted at 10 V bias, so the photocurrents remain relatively stable with the increase of voltage. While the micro-hole diameter is larger than or equal to $6 \mu\text{m}$, the absorption layer at micro-hole cannot be depleted completely in the horizontal direction, as shown in Fig. 2(f). Thus, the depletion region of the absorption layer will gradually become larger and the photocurrent will slowly increase with the increases of the reverse voltage.

The responsivity (R) and corresponding external quantum efficiency (η) can be calculated by the following formulas [22],

$$R = \frac{I_p}{P_{\text{opt}}} = \frac{I_{\text{ph}} - I_d}{P_{\text{opt}}} \quad (1)$$

$$\eta = \frac{1241 R}{\lambda} \quad (2)$$

where I_{ph} and I_d represent the photocurrent and dark current of PDs, respectively. P_{opt} is the optical power in watts. The I_{ph} is four orders of magnitude larger than I_d for any PDs ($I_{\text{ph}} - I_d \approx I_{\text{ph}}$), therefore R depends linearly on I_{ph} . λ is the wavelength in nm.

Fig. 3(a) indicates that the spectral response and external quantum efficiency of the devices at 10 V bias. The device with 4 μm micro-hole exhibited a peak responsivity of 0.159 A/W at 290 nm ($\eta = 68.1 \%$). Its peak responsivity and quantum efficiency are increased by 10.4 % and

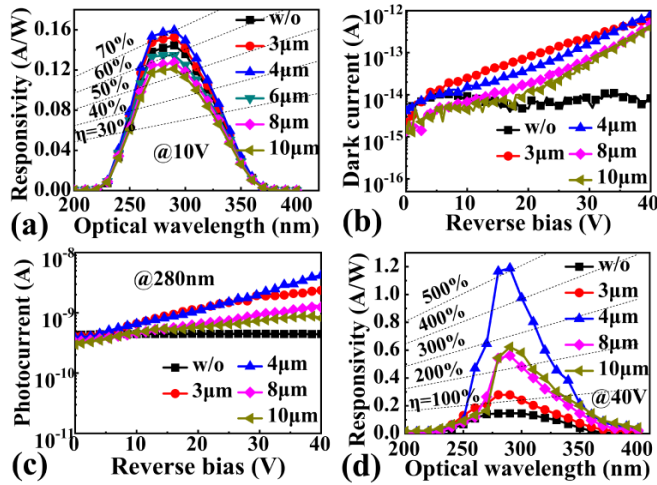


Fig. 3. (a) Spectral response of devices with and without micro-hole at 10 V bias. (b) Dark I-V and (c) photocurrent voltage characteristics at the bias from 0-40 V. (d) Spectral response of devices at 40 V bias.

6.5 %, respectively, compared to the device without micro-hole ($R = 0.144$ A/W and $\eta = 61.6$ %). The micro-hole area of device with 3 μm and 4 μm micro-hole are accounted for 7.7 % and 10.9 % of the single device area, respectively. Therefore, device with 4 μm micro-hole has a larger ratio of micro-hole area to device area than device with 3 μm micro-hole, resulting in more UV light directly absorbed by the i layer and improving the quantum efficiency (η). Nevertheless, it should be noted that the spectral responsivities of devices with micro-holes ($D = 6, 8,$ and 10 μm) decreased because of the absorption layer at the micro-hole cannot be completely depleted. Although the photosensitive area has been increased and the absorption of the p^+ layer has also been reduced, there is no electric field in the middle area of the micro-hole and the photo-generated carriers cannot be separated, which leads to the decrease of spectral response.

As shown in Fig. 3(b) and Fig. 3(c), the dark current and photocurrent of devices without micro-hole remain stable at the bias range of 0-40 V. However, when the reverse bias is greater than 15 V, the dark current and photocurrent of the devices with micro-holes gradually increase. This phenomenon may be due to the local avalanche effect of the device with micro-hole. This effect can be explained that there is a higher electric field in the depletion region near the micro-hole arrays, which lead to electrons and holes could obtain higher kinetic energy, and collide with the crystal lattice of SiC, then generate a large number of electron-hole pairs. The local avalanche effect of the device with micro-holes leads to the increase of both dark current and photocurrent, and the ratio of photocurrent to dark current close to 10^4 when the reverse bias is 40 V. Fig. 3 (d) shows the spectral response of devices with micro-holes under 40 V bias. The peak responsivity and external quantum efficiency of the device with 4 μm micro-hole reach 1.19 A/W and 508 % at 40 V bias, which are 815 % and 819 % higher than that of the device without micro-hole respectively.

To further verify the local avalanche effect occurred in the absorption layer at the micro-holes, the electric field intensity at the micro-hole was simulated by TCAD. According to

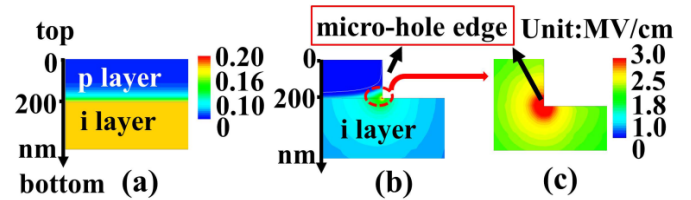


Fig. 4. The electric field intensity distribution diagrams of devices simulated by TCAD at 40 V bias (a) without micro-hole and (b) with micro-hole of 4 μm in diameter and 200 nm in depth. (c) Enlarged view of the micro-hole edge shown in Fig. 4 (b).

Fig. 4 (a), the maximum electric field intensity of the device without micro-hole is 0.2 MV/cm, which is less than the critical breakdown electric field of 4H-SiC (~ 3.0 MV/cm) [23]. As shown in Fig. 4 (b) and (c), the maximum electric field intensity of the device with diameter of 4 μm and depth of 200 nm micro-hole can arrive at 3.0 MV/cm, which is sufficient to induce local avalanche effect. Moreover, there are some regions in the micro-hole with such high electric field intensity, which is likely to cause avalanche breakdown.

As the reverse bias is increased to 40V, the depletion region does not expand, which means the micro-hole still cannot be completely depleted for device with micro-hole diameter larger than or equal to 6 μm . However, devices with micro-hole ($D = 3$ and 4 μm) can be completely depleted at the micro-holes. Moreover, device with 4 μm micro-hole has a larger micro-hole absorption area. The electric field intensity at the edge of the micro-hole has reached the condition of SiC avalanche breakdown, which can prove that the gain at 40V bias comes from the avalanche mechanism. Therefore, considering the change of depletion region and the electric field of the micro-hole edge, the device with 4 μm micro-hole can not only be completely depleted at the micro-hole, but also has adaptive electric field intensity at the edge of the micro-hole, which contributes to a highest responsivity and external quantum. These results indicate that the p-i-n devices with 4 μm micro-hole obtain a remarkable performance at a low voltage (~ 40 V).

In order to obtain large current gain, the fabricated p-i-n devices with micro-hole arrays require relative lower voltage, compared with the conventional APDs that usually operate at avalanche breakdown voltage of higher than 100 V. Besides, the gain of devices obtained at 40 V is reliable and repeatable. And the local avalanche at low voltage is easy to control without quenching circuit, and increases the lifetime of devices.

IV. CONCLUSION

In this letter, 4H-SiC p-i-n UV PDs with periodic micro-hole arrays are fabricated and measured. The 4H-SiC PDs exhibit an average dark current about 6.0×10^{-15} A in the reverse bias range of 0-10 V. Compared to device without micro-hole, the peak responsivity and corresponding external quantum efficiency of device with 4 μm micro-hole under 10 V bias are increased by 10.4 % and 6.5 %, respectively. As the bias increased to 40 V, the peak responsivity and external quantum efficiency increase by 815 % and 819 %, respectively. This research has a great significance to improve the application for weak UV detection.

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